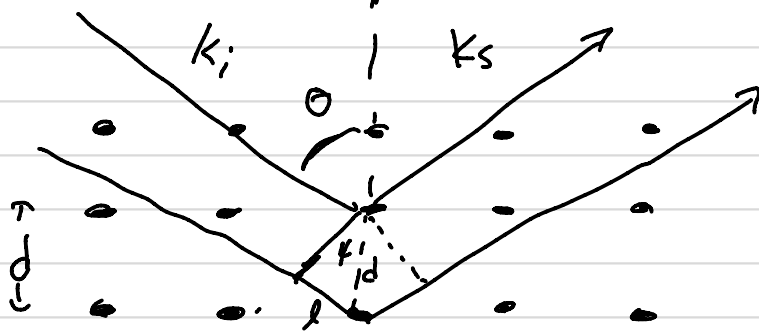


Lecture 8 -

RDFs continued

Last time: characterized liquid/gas structure by  $g(r)$ , the radial distribution function:  $g(r) = \frac{N-1}{4\pi r^2} \langle \delta(r-r') \rangle$

But how do we measure the structure of these systems - do by scattering expt, like for a solid. Recall:



$$l = d \sin \psi$$

$$\text{path dist} = 2l = 2d \sin \psi$$

Constructive interference when  $2d \sin \psi = n \lambda$   
(Bragg Scattering)

For a plane wave,  $\psi(r) = e^{-i\vec{k} \cdot \vec{r}}$ , [ $\vec{k} \cdot \vec{r}$  is phase at a point]

In this scattering experiment, every photon comes in with momentum  $|\vec{k}_i| = 2\pi/\lambda$  and leaves with momentum  $\vec{k}_s$

Phase at  $\vec{r}_1$  is  $-\vec{k}_i \cdot \vec{r}_1$  and  $\vec{r}_2$  is  $-\vec{k}_i \cdot \vec{r}_2$

Phase diff is  $-\vec{k}_i \cdot (\vec{r}_1 - \vec{r}_2) = \delta\phi_i$

$$\delta\phi_i = |\vec{k}| |\vec{r}_1 - \vec{r}_2| \cos\theta \quad \text{where } \theta \text{ is angle}$$

between incoming wave &  $\vec{r}_2 - \vec{r}_1$

$$= 2\pi/\lambda d \cos\theta$$

$$\delta\phi_s = \vec{k}_s \cdot (\vec{r}_1 - \vec{r}_2)$$

$$\delta\phi = \delta\phi_s + \delta\phi_i = (\vec{k}_s - \vec{k}_i) \cdot (\vec{r}_1 - \vec{r}_2)$$
$$= \vec{q} \cdot (\vec{r}_1 - \vec{r}_2)$$

↑  
momentum transfer

for elastic,  $\theta_{in} = \theta_{out}$

$$\delta\theta = 4\pi/\lambda d \cos\theta$$

constructive  $\delta\theta = 2\pi n$

↓ Bragg again

$$\Rightarrow 4\pi/\lambda d \cos\theta = 2\pi n \Rightarrow 2d \cos\theta = n\lambda$$

Turns out, outgoing wave is sum over all scattering events

$$\psi(\vec{q}) = \sum_{j=1}^N f_j e^{-i\vec{q} \cdot \vec{R}_j}$$

pos of particles  
↑  
change in wave vec  
 $\vec{k}_s - \vec{k}_i$

$f_j$  is form factor that depends on how atom interacts w/ light

$$\text{Intensity} = |\psi^* \psi| = \sum_{i=1}^N \sum_{j=1}^N f_i f_j e^{-i\vec{q} \cdot (\vec{R}_j - \vec{R}_i)}$$

The "structure factor" is defined by

normalizing by  $\sum_{i=1}^N f_i^2$

$$S(q) = \frac{1}{\sum_{i=1}^N f_i^2} \sum_i \sum_j e^{-iq \cdot (R_j - R_i)} \cdot f_i \cdot f_j$$

if all the same type,  $f_i = f$

$$\Rightarrow S(q) = \frac{1}{N f^2} \cdot f^2 \sum_{i \neq j} e^{-iq \cdot (R_j - R_i)} = \boxed{\frac{1}{N} \sum_{i \neq j} e^{-iq \cdot (R_j - R_i)}}$$

To actually compute, avg over mc motions

$$S(q) = \left\langle \frac{1}{N} \sum_{i \neq j} e^{-iq \cdot \Delta R} \right\rangle = \frac{1}{N} \left\langle \left| \sum_i e^{iq \cdot R_i} \right|^2 \right\rangle$$

↑  
rewrite

± doesn't matter

separate into self,  $i=j$ ,  $R_i - R_j = 0$  & distinct

$$S(q) = 1 + \frac{1}{N} \left\langle \sum_{i \neq j} e^{-iq \cdot (\vec{R}_j - \vec{R}_i)} \right\rangle$$

↑  
N · (N-1) terms  $e^{iq \cdot (\vec{R}_j - \vec{R}_i)}$   
 $\langle e^{iq \cdot (\vec{R}_j - \vec{R}_i)} \rangle = \langle e^{iq \cdot (\vec{R}_2 - \vec{R}_1)} \rangle$  avg value  
 doesn't depend on particle pair

$$\Rightarrow S(q) = 1 + (N-1) \langle e^{-iq \cdot (\vec{R}_2 - \vec{R}_1)} \rangle$$

$$= 1 + (N-1) \cdot \frac{\int dR_1 dR_2 \dots dR_N e^{-iq \cdot (\vec{R}_2 - \vec{R}_1)} e^{-\beta U(\vec{x})}}{\mathcal{Z}}$$

$$= 1 + (N-1) \cdot \int dR_1 \int dR_2 e^{-iq \cdot (R_2 - R_1)} \underbrace{\frac{\int dR^{N-1} e^{-\beta U(\vec{x})}}{\mathcal{Z}}}_{\frac{\rho^2 g^2(R_1, R_2)}{N \cdot N - 1}}$$

switched to k

↓

$$S(k) = 1 + \frac{1}{N} \cdot \int d\vec{r}_1 \int d\vec{r}_2 \rho^2 g(\vec{r}_1, \vec{r}_2) e^{-ik(\vec{r}_2 - \vec{r}_1)}$$

$$= 1 + \frac{1}{N} \int d\vec{R} d\vec{r} \rho^2 g(\vec{r}, \vec{R}) e^{ik\vec{r}} \quad \vec{r} = \vec{r}_2 - \vec{r}_1$$

defined  $\int d\vec{R} g(\vec{r}, \vec{R}) = V g(\vec{r})$

$$= 1 + \frac{1}{\rho} \int d\vec{r} \rho^2 g(\vec{r}) e^{-ik\vec{r}}$$

$$= 1 + \rho \int d\vec{r} g(\vec{r}) e^{-ik\vec{r}}$$

Reminder:  $\tilde{f}(k) = FT[f(x)] = \int_{-\infty}^{\infty} dx e^{-ikx} f(x)$

$$= 1 + \rho \int_0^{\pi} d\theta \int_0^{2\pi} d\phi \int_0^{\infty} dr r^2 \sin\theta g(r) e^{-ikr \cos\theta}$$

$$u = \cos\theta$$

$$du = -\sin\theta d\theta$$

$$= 1 + 2\pi\rho \int_{-1}^1 du \int_0^{\infty} dr r^2 g(r) e^{+ikru}$$

$$\int e^{ax} = \frac{1}{a} e^{ax}$$

$$= 1 + 2\pi\rho \int_0^{\infty} dr r^2 g(r) \cdot \frac{1}{ikr} \cdot \left[ e^{+ikru} \right]_{u=-1}^1$$

$$\frac{e^{+iak} - e^{-iak}}{2i} = +\sin(ak)$$

$$= 1 + 4\pi\rho \int_0^{\infty} dr \cdot r^2 g(r) \frac{\sin(kr)}{kr}$$

← can predict  $S(k)$  from liquid struct

# Thermodynamic Quantities from $g(r)$

Very interesting result:  $g(r) = e^{-\beta w(r)}$

Reversible work theorem,  $w(r)$  is work to move two particles from infinite separation to separation  $r$  - reversibly,  $(\text{const } N, V, T)$

Work =  $\Delta A$  in process

work done by the force =  $\int_{+\infty}^r F(r) dr$ , work you have to do =  $\int_r^{\infty} F(r) dr$

But what is  $F$ ? ,  $-\nabla U(r)$  averaged over positions of other particles, if reversibly slow

$$\begin{aligned} \left\langle -\frac{\partial U(r_{12})}{\partial r_{12}} \right\rangle &= \frac{\int dr_3 dr_4 \dots dr_N \frac{-dU}{dr_{12}} e^{-\beta U(r)} }{\int dr_3 dr_4 \dots dr_N e^{-\beta U(r)}} \\ &= \int dr^{N-2} \frac{1}{\beta} \frac{d}{dr_{12}} e^{-\beta U(r)} / \int dr^{N-2} e^{-\beta U(r)} \\ &= k_B T \frac{d}{dr_{12}} \log \left[ \int dr^{N-2} e^{-\beta U(r)} \right] \end{aligned}$$

$$\begin{aligned} \left[ g^{(2)}(r_1, r_2) = z \rho^2 \cdot \frac{1}{N(N-1)} \int dr^{N-2} e^{-\beta U(r)} \right] \\ = k_B T \frac{d}{dr_{12}} \log (g^{(2)}(r_1, r_2)) = k_B T \frac{d}{dr} \log (g(r)) \end{aligned}$$

$$\Rightarrow w(R) = \int_R^\infty k_B T \left[ \frac{d}{dr} \log g(r) \right] dr$$

$$= k_B T \log g(r) \Big|_R^\infty = 0 - \underline{k_B T \log g(R)}$$

$$\Rightarrow g(R) = e^{-\beta w(R)}$$

$w(R)$  is called the "potential of Mean force"  $\rightarrow \langle -\frac{\partial U}{\partial r} \rangle = -\frac{d}{dr} w(r)$

and it is what we

often want to calculate in free energy methods & what we fit for coarse grained forces

Example

